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Patentanmeldung Nr. Patent application No. Demande de brevet n°

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Der Präsident des Europäischen Patentamts;
Im Auftrag

For the President of the European Patent Office

Le Président de l'Office européen des brevets
p.o.

I.L.C. HATTEN-HECKMAN

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**Blatt 2 der Bescheinigung
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Method of measuring alignment of a substrate with respect to a reference alignment mark
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The invention relates to a method of measuring alignment of a substrate, provided with at least one substrate alignment mark having a periodic structure, with respect to a reference alignment mark, having a periodic structure, prior to imaging a mask pattern in a resist layer on the substrate, which method comprises the steps of:

5 - illuminating a substrate alignment mark with an alignment beam and imaging this mark on a reference mark, and
- determining the intensity of alignment radiation from the reference mark.

The invention also relates to a method of manufacturing devices by means of a lithographic projection apparatus which method comprises the method of measuring
10 alignment.

The lithographic projection apparatus is an essential tool in the manufacture of integrated circuits (IC's) by means of diffusion and masking techniques. By means of this 15 apparatus, a number of masks having different mask patterns are successively imaged at the same position on a semiconductor substrate. The substrate must undergo the desired physical and chemical changes between the successive successive projections of the different mask patterns. To that end, the substrate must be removed from the apparatus after it has been exposed with a mask pattern. After it has undergone the desired process steps, the substrate 20 must be placed again in the apparatus at the same position so as to expose it with a second mask pattern, and so forth. Thereby it must be ensured that the second and subsequent mask patterns are positioned accurately with respect to device structures already formed in the substrate. To this end the lithographic projection apparatus is provided with an alignment system with which alignment marks on the substrate are aligned with respect to alignment 25 marks on the mask. This alignment system comprises an optical alignment-measuring device for measuring deviations in this alignment.

Alignment of a substrate with respect to a mask may be measured with the so-called on-axis method, whereby a substrate alignment mark is directly imaged on a mask alignment mark via the projection lens of the apparatus. This method is also known as the

through-the-lens (TTL-) method. The alignment may also be measured by the off-axis method, whereby a substrate alignment mark is imaged on a reference alignment mark outside the field of the projection system of the apparatus. In a very promising embodiment of the off-axis method a substrate alignment mark is aligned with respect to an alignment

5 mark on the substrate holder via reference mark that is arranged outside the projection column. During this first alignment step, the substrate holder with the substrate is positioned outside the projection column. After the first alignment step has been performed, the substrate holder is positioned in the projection column and in a second alignment step the substrate alignment mark is imaged via the projection lens on a mask alignment mask.

10 A lithographic projection apparatus may not only be used for the manufacture of IC's but also for the manufacture of other structures having structure details of the order of 1 μ m and smaller. Examples are structures of integrated, or planar, optical systems, guiding and detection patterns of magnetic domains memories, structures of liquid crystal display panels and magnetic heads. Also in the manufacture of these structures, images of mask 15 patterns must be aligned very accurately with respect to a substrate.

The lithographic projection apparatus may be a stepping apparatus or a step-and-scan apparatus. In a stepping apparatus, the mask pattern is imaged in one run on an IC area of the substrate. Subsequently, the substrate is moved with respect to the mask in such a way that a subsequent IC area will be situated under the mask pattern and the projection lens 20 system and the mask pattern is imaged on the subsequent IC area. This process is repeated until all IC areas of the substrate are provided with a mask pattern image. In a step-and-scan apparatus, the above-mentioned stepping procedure is also followed, but the mask pattern is not imaged in one run but via scanning movement. During imaging of the mask pattern, the substrate is moved synchronously with the mask with respect to the projection system and the 25 projection beam, taking the magnification of the projection system into account. A series of juxtaposed partial images of consecutively exposed parts of the mask pattern is imaged in an IC area. After the mask pattern has been completely imaged in an IC area, a step is made to a subsequent IC area. A possible scanning procedure is described in the article: "Sub-micron 1:1 Optical Lithography" by D.A. Markle in the magazine "Semiconductors International" of 30 May 1986, pp. 137-142.

US Patent 4,251,160 discloses an optical lithographic projection apparatus intended for the manufacture of IC's and provided with a single on-axis alignment unit. The substrate- and mask alignment marks are gratings. A double on-axis alignment unit for aligning a first and second substrate alignment mark with respect to a first and second mask

alignment mark, respectively, is disclosed in US Patent 4,778,275. Patent application WO 98/39689 discloses an off-axis alignment unit and US Patent 5,243,195 discloses an alignment system comprising both an on-axis alignment unit and an off-axis alignment unit.

5 The above-mentioned alignment methods and units has hitherto worked to full satisfaction, but it is to be expected that these methods may present problems with regard to accuracy and reliability when the structure details, or line widths, decrease and when novel technologies are used in the IC manufacture.

In connection with the increasing number of electronic components per unit of surface area of IC's and the resultant smaller dimensions of these components, increasingly 10 stricter requirements are imposed on the accuracy with which integrated circuits are made. The positions where the successive mask patterns are imaged on the substrate must therefore be controlled more and more accurately. In the manufacture of new-generation IC's with smaller line widths, the alignment accuracy will have to be improved or, in other words, it must be possible to detect smaller alignment deviations so that the resolving power of the 15 alignment system must be increased.

On the other hand stricter requirements must also be imposed on the planeness of the substrate due to the required higher numerical aperture (NA) of the projection system in the case of decreasing line widths. The depth of focus of the projection system decreases as the NA increases. Since some image field curvature occurs at the desired large image field 20 of the projection system, there is hardly any room left for unevenness of the substrate. To obtain a substrate that is sufficient plane, it has been proposed to polish the substrate by means of the chemical mechanical polishing (CMP) process between two consecutive exposures with different mask patterns in the projection apparatus. However, this polishing process affects the accuracy of the on-axis alignment method.

25 Furthermore, the manufacturing process for the new-generation IC's is becoming more and more complicated; the number of process steps and the number of process layers on the substrate increase more and more. Some of these layers also introduce asymmetries in the substrate grating alignment mark and hence alignment errors.

30

It is an object of the present invention to provide a method of measuring alignment of a substrate with respect to a reference according to the opening paragraph, which method is more accurate and reliable than known methods and provides an alignment

signal which is less sensitive to the said effects. To that end the method is characterized by the steps of:

- using a substrate alignment mark having a periodic structure with a period p_1 substantially smaller than the period of the reference alignment mark;

5 - providing the resist layer with an additional alignment mark having a periodic structure with a period p_2 such that, upon illumination by the alignment beam of the substrate alignment mark and the additional alignment mark, an interference pattern is generated having a period substantially equal to the period of the reference alignment mark, and

- imaging the interference pattern on the reference alignment mark

10 A substrate is to understood to mean a plate of material, for example silicon, into which a complete device, such as an IC is to be formed level wise by means of a number of successive sets of processing steps. Each of these sets comprises as main processing steps: applying a resist layer on the substrate, aligning the substrate with a mask, imaging the pattern of this mask in the resist layer, developing the resist layer, etching the substrate via the resist layer and further cleaning- and other processing steps. The term substrate covers substrates at different stages in the device manufacturing process, i.e. both a substrate having only one layer of device features and a substrate having all but one layer of device features, and all intermediate substrates. All these substrate have in common that they are provided with at least one alignment mark visible to the alignment beam.

20 The periods p_1 and p_2 of the substrate alignment mark and the additional alignment mark, respectively are preferably of the order of resolving power of the projection system and much smaller than the period of a conventional substrate alignment mark.

Because of the smaller periods, smaller alignment errors can be measured with the new method. The period of the interference pattern, or Moiré pattern, is determined by the periods 25 of the substrate- and additional alignment marks. By a proper choice of the period p_1 and p_2 , the period of the interference pattern can be made equal to the period of a conventional substrate alignment mark so that the method can be carried out with a conventional alignment system. The actual alignment errors are magnified by the new method and a small alignment error results in a considerably larger displacement of the interference pattern with respect to

30 the reference alignment mark and in a considerable change in the alignment signal from the alignment unit. This means that less interpolation of alignment signal is needed and that a considerably more accurate measurement becomes possible. As the alignment signal provided by the new method is an averaged signal over a relative large area, this signal is less sensitive to local surface deformations.

It is remarked that US Patent 5,414,514 discloses the use of an interference pattern to measure the alignment of two plates, which pattern is obtained when superposed first and second grating alignment marks having periods p_1 and p_2 , respectively are illuminated. The first alignment mark is a substrate alignment mark. However the second 5 alignment mark is a wafer alignment mark and not an additional alignment mark in a layer on the substrate. The interference pattern is not imaged on a reference alignment mark but on a CCD sensor. The substrate and the mask are separated by only a small gap and the mask pattern is imaged on the substrate not by a projection system but by a proximity printing process using X-rays.

10 In the article: "Submicrometer lithographic alignment and overlay strategies" in SPIE, Vol 1343, X-ray/ EUV Optics for Astronomy, Microscopy, Polarimetry and Projection Lithography" (1990) pp.245-255 it is stated that Moiré techniques may be an effective technique for alignment and overlay registration in photolithography. This article discusses only how two gratings having slightly different grating periods or grating line orientations 15 form a Moiré pattern. It does not enter into the alignment method itself and does not disclose that the resolving power and accuracy of a conventional alignment system can be increased considerably by the Moiré technique.

20 For determining the mutual shift of the substrate alignment mark and the additional alignment mark from the position of the image of the interference pattern with respect to the reference alignment mark a further reference mark is needed. An embodiment 25 of the measuring method, wherein such further reference mark is used, is characterized in that, use is made of a substrate reference alignment mark having substantially the same period as the interference pattern, that the substrate reference alignment mark is imaged on the reference alignment mark and in that the difference between the positions of the image of the interference pattern and that of the substrate reference alignment mark with respect to the reference alignment mark is determined. Said difference between the positions is a measure for the shift between the substrate alignment grating and the additional alignment grating. The substrate reference mark may be constituted by a substrate global alignment mark.

30 The alignment marks used with the measuring method may have different structures, provided that they are periodic. The so-called Siemens star is such a periodic alignment mark that is already used in the optical lithography technique.

Preferably the method is characterized in that, use is made of gratings for the substrate-, the additional- and the reference alignment marks.

Grating structures have been proven to be very suitable as alignment marks.

The additional alignment mark is formed in the resist layer by imaging a corresponding mark provided on the mask outside the mask pattern in the resist layer by means of the lithographic apparatus. The area of the substrate layer where the mark image is located may be developed and the developed mark image used for carrying out the measuring 5 method. Preferably the method is characterized in that the additional alignment mark is a latent mark

A latent mark is understood to mean a latent, or non-developed, image of an alignment mark. A resist layer with such a latent image comprises areas, which are linear areas in case of a grating mark, which have another phase effect on an incident beam than their 10 surroundings. These effects are due to the intensity variations in the beam that images the mark, which variations cause local changes of the refractive index in the layer and local shrinkage of this layer. Due to these phase effects the latent alignment mark is discernible by the alignment beam. The advantage of using a latent alignment mark is that the substrate with the mark image in the resist layer needs not to be removed from the lithographic apparatus 15 for developing this image.

If a latent additional alignment mark is used a second aspect of the invention can be realized. This aspect relates to a new method of aligning a substrate with respect to a mask, which method uses a global alignment measuring method to measure the position of a global substrate alignment mark with respect to a global reference alignment mark. This 20 method is characterized by the steps of:

- providing a substrate with a substrate reference alignment mark and with a substrate fine alignment mark having a period substantially smaller than that of the substrate reference alignment mark, which substrate is covered with a resist layer;
- aligning the substrate reference alignment mark with respect to a non-substrate 25 reference alignment mark using a coarse alignment measuring method;
- providing the resist layer with an additional alignment mark having a period of the same order as that of the substrate fine alignment mark;
- measuring the alignment of the substrate fine alignment mark with respect to the additional alignment mark by illuminating these two marks and imaging the resulting 30 interference pattern on the non-substrate reference alignment mark, and using the measuring signal of this measurement to correct the signal obtained with the coarse alignment method.

The substrate reference alignment mark may be a global alignment mark or an alignment mark belonging to an IC area of the substrate. The non-substrate reference

alignment mark may be a mask global alignment mark or a mark outside the mask. A global alignment mark is understood to mean a conventional periodic alignment mark for aligning a substrate as such with respect to a reference alignment mark such as a masker alignment mark. The period of the global alignment mark is substantially larger than the resolution limit of the projection system by means of which the global substrate alignment mark is imaged on the wafer alignment mark, which in principle is a global alignment mark.

The invention may be implemented in different ways resulting in different embodiments of the measuring method. A first embodiment is characterized in that it is based on the on-axis alignment principle.

In this embodiment the interference pattern is imaged on a mask alignment mark by means of the projection system that is intended for projecting mask patterns onto the substrate.

This embodiment is preferably further characterized in that the interference pattern is imaged on a mask alignment mark via an optical filter, which selects diffraction orders of the radiation from the substrate alignment marks to proceed to the said mask alignment mark.

This optical filter, or diaphragm, prevents noise radiation, for example caused by false reflection at components in the apparatus, from reaching the detector. By selecting, for example only the first diffraction orders for imaging the interference pattern on the mask alignment mark, the accuracy of the alignment measurement can be increased by a factor of two.

A second embodiment of the method is characterized in that it is based on the off-axis alignment principle.

The interference pattern is imaged on a reference alignment mark forming part of an off-axis alignment device that is located next to the projection lens. With this device a number of diffraction orders of the alignment radiation from the substrate, for example the first to the seventh order, can be detected separately. The mask is also aligned with respect to the off-axis alignment device, so that the substrate and the mask are aligned in an indirect, or two-step, way. An advantage of this off-axis alignment method is that it is largely insensitive to CMP process parameters.

An off-axis alignment is performed also in lithographic projection apparatus having two substrate stages and a separate measuring station in addition to the projection station. During projection of a mask pattern on a first substrate in the projection station the position of a second substrate is measured in the measuring station. An embodiment of such

apparatus, wherein two substrate stages commute between the measuring station and the projection station is shown in US-A 4,861,162. Such apparatus has the advantage that its throughput, i.e. the number of substrates that can be processed per time unit, is considerably larger than that of a comparable apparatus having only a projection station and no measuring station. The alignment measuring method of the present invention may be used in the measuring station.

This invention also relates to a method for manufacturing devices in at least one layer of a substrate, which method comprises at least one set of the following successive steps of:

- 10 - aligning a mask provided with a mask pattern comprising pattern features corresponding to device feature to be configured in said layer;
- imaging, by means of projection radiation, the mask pattern in a radiation sensitive layer on the substrate, and
- removing material from, or adding material to, areas of said layer and substrate, which areas are delineated by the mask pattern image. This method is characterized in that the alignment is carried out by means of the alignment measuring method as described herein above.

20 These and other aspects of the invention are apparent from and will be elucidated, by way of non-imitative example, with reference to the embodiments described hereinafter

In the drawings:

Fig.1 shows an embodiment of a lithographic projection apparatus for repetitively imaging a mask pattern on a substrate;

Fig.2 shows an embodiment of a global substrate alignment mark;

Fig.3 shows an embodiment of a double alignment-measuring device by means of which the novel alignment method can be performed;

30 Fig.4 shows an embodiment of a fine substrate alignment mark and an additional alignment mark provided in a substrate and resist layer, respectively;

Fig.5 shows an enlarged cross-section of these marks;

Fig.6 shows the flow diagram of a novel alignment strategy;

Fig.7 shows an order filter of the on-axis alignment measuring device and first-order sub-beams generated by the fine alignment marks, and

Fig.8 shows an embodiment of an off-axis alignment-measuring device by means of which the novel alignment method can be performed.

5 Fig.1 shows the principle and an embodiment of a lithographic projection apparatus for repetitively imaging a mask pattern on a substrate. The main components of this apparatus are a projection column, in which a mask MA provided with a mask pattern C to be imaged is arranged and a movable substrate table WT, by means of which the substrate W can be positioned with respect to the mask pattern. The apparatus further comprises an
10 illumination unit, which consists of a radiation source LA, for example a Krypton-Fluoride laser, a lens system LS, a reflector RE and a condenser lens CO. The projection beam PB supplied by the illumination unit illuminates the mask pattern C present in the mask MA which is arranged on a mask holder (not shown) in the mask table MT.

15 The projection beam PB passing through the mask pattern C traverses a projection lens system PL arranged in the projection column and shown only diagrammatically. This projection system forms an image of the pattern C successively in each of the IC areas, or substrate fields, of the substrate W. The projection lens system has, for example a magnification M of $\frac{1}{4}$, a numerical aperture of the order of 0,5, or larger, and a diffraction-limited image field with a diameter of the order of 0,25. These numbers are
20 arbitrary and may vary with every new generation of the projection apparatus. The substrate W is arranged in a substrate holder (not shown) which forms part of a substrate table WT supported in, for example, air bearings. The projection lens system PL and the substrate table WT are arranged in a housing HO which is closed at its lower side by a base plate BP of, for example granite, and at its upper side by the mask table MT.

25 As is shown in the top-right-hand corner of Fig. 1, the mask has two alignment marks M_1 and M_2 . These marks preferably consist of diffraction gratings, but they may be alternatively formed by other periodical structures. The alignment marks are preferably two-dimensional, i.e. they extend in two mutually perpendicular directions, the X and Y directions in Fig.1. The substrate W, for example a semiconductor substrate or wafer,
30 comprises a plurality of alignment marks, preferably also two-dimensional diffraction gratings, two of which P_1 and P_2 , are shown in Fig.1. The marks P_1 and P_2 are located outside the substrate fields where the images of the mask pattern must be formed. The substrate alignment marks P_1 and P_2 are preferably formed as phase gratings and the mask alignment marks M_1 and M_2 are preferably formed as amplitude gratings.

Fig.2 shows one of the two identical substrate phase gratings on a larger scale.

Such a grating may comprise four sub-gratings $P_{1,a}$, $P_{1,b}$, $P_{1,c}$ and $P_{1,d}$, two of which, $P_{1,b}$ and $P_{1,d}$, are used for measuring alignment in the X direction and the two other sub-gratings, $P_{1,a}$ and $P_{1,c}$ are used for measuring alignment in the Y direction. The two sub-gratings $P_{1,b}$ and

5 $P_{1,c}$ have a grating period of, for example, 16 μm and the sub-gratings $P_{1,a}$ and $P_{1,d}$ have a grating period of, for example, 17,6 μm . Each sub-grating may cover a surface area of, for example, $200 \times 200 \mu\text{m}^2$. An alignment accuracy which, in principle, is less 0,1 μm can be achieved with these grating marks and a suitable optical system. Different gating period for the sub-gratings have been chosen so as to increases the capture range of the alignment-measuring device.

10 Fig.1 shows a first embodiment of an alignment-measuring device, namely a double alignment-measuring device. In this device two alignment beams b and b' are used for measuring the alignment of the substrate alignment mark P_2 with respect to the mask alignment mark M_2 , and the substrate alignment mark P_1 with respect to the mask alignment 15 mark M_1 , respectively. The alignment measuring beam b is reflected to the reflective surface 27 of a prism 26 by means of a reflective element 30, for example, a mirror. The surface 27 reflects the beam b to the substrate alignment mark P_2 which sends a part of the radiation as beam b_1 to the associated mask alignment mark M_2 where an image of the mark P_2 is formed. A reflecting element 11, for example a prism, which directs the radiation, passed by the mark 20 M_2 to a radiation-sensitive detector 13 arranged above the mark M_2 .

The second alignment measuring beam b' is reflected to a reflector 29 in the projection lens system PL by a mirror 31. This reflector sends the beam b' to a second reflecting surface 28 of the prism 26, which surface directs the beam b' onto the substrate alignment mark P_1 . This mark reflects a part of the radiation of the beam b' as a beam b_1' to the mask alignment mark M_1 where an image of the mark P_1 is formed. The radiation of the beam b_1' passing through the mark M_1 is directed towards a radiation-sensitive detector 13' by a reflector 11'. The operation of the double alignment-measuring device will be further described with reference to Fig.3 showing a further embodiment of such a device.

25 The projection apparatus further comprises a focus error detection system for determining a deviation between the image plane of the projection lens system PL and the surface of the substrate W. A measured deviation can be corrected, for example, by moving the projection lens system with respect to the substrate holder along the optical axis of the projection lens system. The focus error detection system may be constituted by the elements 40-46, which are arranged in a holder (not shown) which is fixedly connected to the holder of

the projection lens system. Element 40 is a radiation source, for example a diode laser, emitting a focus-detection beam b_3 . This beam is directed to the substrate W at a small angle by a reflecting prism 42. The focus detection beam reflected by the substrate is directed to a retroreflector 44 by a prism 43. The retroreflector reflects the beam in itself, so that the focus-detection beam once more transverses the same path, now as beam b_3' , via reflection on the prism 43 to the substrate and from this substrate to the prism 42. The reflected focus-detection beam then reaches a beam splitter 41, which reflects the beam to a further reflector 45. This reflector sends the focus-detection beam to a radiation-sensitive detection system 46. This detection system consists of, for example a position-sensitive detector or of two separate detectors. The position of the radiation spot formed by the beam b_3' on this system is dependent on the extent to which the image plane of the projection lens system coincides with the surface of the substrate W. For an extensive description of the focus error detection system, reference is made to US-A 4,356,392

Instead of this focus detection system with a monochromatic focus-detection beam, a focus-and-tilt detection system with a broadband beam is preferably used. Such a broadband focus detection system is described in US-A 5,191,200.

In order to determine the X and Y positions of the substrate very accurately, the apparatus comprises a composite interferometer system having a plurality of measuring axis, of which only a one-axis sub-system is shown in Fig.1. This sub-system comprises a radiation source 50, for example a laser, a beam splitter 51, a stationary reference mirror 52 and a radiation-sensitive detector 53. The beam b_4 emitted by the source 50 is split by the beam splitter into a measuring beam $b_{4,m}$ and $b_{4,r}$. The measuring beam reaches the measuring mirror in the form of a reflective surface of the substrate table, or preferably a reflective side surface of the substrate holder which forms part of the substrate table and on which the substrate is rigidly secured. The measuring beam reflected by the measuring mirror is combined by the beam splitter 51 with the reference beam reflected by the reference mirror 52 so as to form an interference pattern at the location of the detector 53. The composite interferometer system may be implemented as described in US-A 4,251,160 and then comprises two measuring axes. The interferometer system may alternatively comprise three measuring axes as described in US-A 4,737,823, but is preferably a system with at least five measuring axes as described in EP-A 0 498 499.

By making use of a substrate position detection system in the form of a composite interferometer system the positions of, and the mutual distances between, the alignment marks P_1 and P_2 and the marks M_1 and M_2 can, during alignment, be fixed in a

system of co-ordinates defined by this interferometer system. Thus it is not necessary to refer to a frame of the projection apparatus or to a component of this frame, so that variations in this frame due to, for example temperature variations, mechanical creep and the like do not affect the measurements.

5 Fig.3 shows the principle of the double alignment system with reference to an embodiment which is distinguished from that of Fig.1 by a different manner of coupling the alignment beams b and b' into the projection lens system. The double alignment device comprises two separate and identical alignment systems AS_1 and AS_2 which are positioned symmetrically with respect to the optical axis AA' of the projection lens system PL . The 10 alignment system AS_1 is associated with the mask alignment mark M_2 and the alignment system AS_2 is associated with the mask alignment mark M_1 . The corresponding elements of the two alignment systems are denoted by the same reference numerals, those of the elements of the system AS_2 being distinguished by their primed notation.

15 The structure of the system AS_1 as well as the way in which the mutual position of the mask alignment mark M_2 and, for example, the substrate alignment mark P_2 is determined will now be described first.

20 The alignment system AS_1 comprises a radiation source 1, which emits an alignment beam b . This beam is reflected towards the substrate by a beam splitter 2. The beam splitter may be a partially transparent reflector or a partially transparent prism, but is preferably a polarization-sensitive splitting prism, which is succeeded by a quarter-wavelength plate 3. The projection lens system PL focuses the alignment beam b to a small radiation spot V having a diameter of the order of 1mm on the substrate W . This substrate reflects a part of the alignment beam as beam b_1 in the direction of the mask MA . The beam b_1 traverses the projection lens system PL , which system images the radiation spot on the 25 mask. Before the substrate is arranged in the projection column, it has been pre-aligned in a pre-alignment station, for example the station described in US-A 5,026,166, so that the radiation spot V is located on the substrate alignment mark P_2 . This mark is the imaged by the beam b_1 on the mask alignment mark M_2 . The dimensions of the mask alignment mark M_2 are adapted to that of the substrate alignment mark P_2 , taking the magnification M of the 30 projection lens into account. The image of the mark P_2 then accurately coincides with the mark M_2 if the two marks are mutually positioned in the correct manner.

On their paths to and from the substrate W , the alignment measuring beams b and b_1 have traversed twice the quarter-wavelength plate 3 whose optical axis extends at an angle of 45^0 to the direction of polarization of the linearly polarized beam coming from the

source 1. The beam passing through the plate 3 then has its direction of polarization rotated over 90° with respect to that of the beam b, so that the polarization-sensitive prism 2 passes the beam b1. The use of the polarization-sensitive prism in combination with the quarter-wavelength plate provides the advantage of a minimum radiation loss when coupling the 5 alignment-measuring beam into the radiation path of the alignment system.

The beam b1 passed by the alignment mark M2 is reflected by a prism 11 and directed, for example, by a further reflecting prism 12 towards a radiation-sensitive detector 13. This detector is, for example, a composite photodiode having, for example, four separate radiation-sensitive areas in conformity with the number of sub-gratings according to Fig.2.

10 The output signals of the sub-detectors comprise information about the extent to which the mark M2 coincides with the image of the mark P2. These signals may be processed electronically and used for moving the mask with respect to the substrate by means of driving systems (not shown) so that the image of the substrate alignment mark P2 coincides with the mask alignment mark M2.

15 A beam splitter 4 splitting a part of the beam b1 is beam b2 may be arranged between the prism 11 and the detector 13. The split beam is then incident via, for example, two lenses 16 and 16 on a television camera, which is coupled to a monitor (not shown) on which the alignment marks P2 and M2 are visible to an operator of the lithographic apparatus.

Analogously as described above for the alignment marks P2 and M2, the marks 20 M1 and P1 and M1 and P2, respectively, can be aligned with respect to each other. The alignment-measuring system AS2 is used for the last-mentioned alignments.

The alignment marks P1 and P2 in the form of gratings or other diffraction elements split the alignment-measuring beams incident thereon in a non-deflected zero-order sub-beam and a plurality of, deflected, first-order and higher-order sub-beams. Of these sub-beams only those having the same diffraction order are selected in the alignment-measuring 25 system for imaging a substrate alignment mark on a mask alignment mark. For the selection of the sub-beams, an order diaphragm is arranged in the projection lens system at a position where the sub-beams diffracted in the different diffraction orders are spatially separated to a sufficient extent, for example, in the Fourier plane of the projection system. This order 30 diaphragm is diagrammatically indicated by means of the reference numeral 25 in Fig.3 and consists of a plate, which is non-transitive to the alignment-measuring radiation and has a plurality of radiation-transitive apertures or areas. If the alignment marks have a two-dimensional structure, the plate has four apertures: two for the sub-beams diffracted in the relevant order in the plus and minus X direction and two for the sub-beams diffracted in the

relevant order in the plus and minus Y direction. Moreover, an additional order diaphragm improving the selection of the desired order is preferably arranged in the detection branch, i.e. the part of the radiation path from the mask alignment mark to the detector 13, 13'. The sub-beams diffracted in the first orders are preferably used for the alignment.

5 The smallest alignment error that can be measured with this system and method, i.e. the resolving power of the system, is determined by the grating period, whereby the measurable error can be decreased to a certain degree by interpolation of the alignment signal. The accuracy of the method is limited by the quality of the grating structures. This quality may be affected by local surface deformations of the substrate and by lithographic 10 processing steps, resulting in, for example PICO, RICO and WICO. These artifacts are offsets in the overlay signal caused by the large coherence length of the measuring beam, for example a He-Ne laser beam. Because of the large coherence length, laser radiation that has been affected by optical components in the system may interfere with the desired signal radiation, i.e. radiation of the plus and minus first orders in the described embodiment. The 15 resulting artifacts may be induced by polarization effects of the mask, or reticle (polarization induced coherence offset: PICO), by the thickness of the reticle (reticle induced coherence offset: RICO) and by the Z-position of the substrate, or wafer (wafer induced coherence offset: WICO).

According to the invention the resolving power of the method and its accuracy 20 can be considerably increased by using a substrate alignment mark P_{10} having a grating period considerably smaller than those of substrate alignment marks used up to now and by using an additional alignment mark P_{11} arranged close to the mark, as shown in Fig.4. This Figure shows a small part of the substrate W comprising the substrate alignment mark P_{10} in cross-section. The additional alignment mark P_{11} is arranged in a resist layer RL on top of the 25 substrate. The substrate alignment mark and the additional alignment mark have a grating period PE_{10} and PE_{11} , respectively, which are preferably of the order of the resolving power, or resolution, of the projection lens system. These grating periods are slightly different, as illustrated in Fig.5.

The upper part of Fig 5 shows a part of the alignment marks in cross-section 30 and on a very enlarged scale. These alignment marks are constituted by phase structures, for example phase gratings. The grating period PE_{10} of the substrate alignment mark is larger than this period P_{11} of additional alignment mark, or the other way round. When illuminating these alignment marks by an alignment-measuring beam the phase effects of these marks on the beam interfere so that an interference phase pattern, or phase image is generated. This

phase pattern, which may also be called a beat pattern or beat grating, has a beat period PE_b which is given by:

$$1/PE_b = 1/PE_{10} - 1/PE_{11}.$$

5

The graph 60 in the lower part of Fig.5 shows the variation of the average phase depth APD of the phase pattern along the x direction, i.e. perpendicular to the grating strips of the fine substrate- and the additional alignment grating. The phase variation or the position of the maxima and minima of the beat pattern is determined by the mutual position of the fine alignment gratings. In order to measure this mutual position or the mutual shift in the X direction of the fine alignment gratings, the beat phase pattern is imaged on a on-axis- or off-axis measuring grating, or -mark, arranged in front of a radiation-sensitive detector. If for this imaging an optical system is used which can resolve the coarse beat pattern with the period PE_b , but not the fine alignment marks with the periods PE_{10} and PE_{11} , only the sine-like variation of the phase pattern, i.e. the position of the beat pattern will be detected. In order to determine the shift of the fine alignment marks relative to each other from the position of the beat pattern, the latter position with respect to the measuring mark can be compared with the position of the substrate mark with respect to the same measuring mark. The substrate reference mark may be constituted by a global alignment mark arranged in the substrate in the neighborhood of the fine alignment mark. The measuring mark is a mask global alignment mark in case of an on-axis alignment device. From the mutual position of the reference mark and the beat pattern the mutual position of the fine substrate and additional mark can be determined in a simple way. A shift of the additional mark over $PE_{11}/2$ relative to the fine substrate mark results in a shift of the beat pattern over $PE_b/2$.

A small shift of the fine alignment marks is thus translated into a considerably larger shift of the beat pattern, i.e. this shift is magnified. The magnification factor M_f is given by:

$$M_f = \text{shift}_{\text{beat}} / \text{shift}_{\text{fine marks}} = PE_{10} / (PE_{11} - PE_{10})$$

30

Because of the magnification, in the alignment signal processing less interpolation of the detector signal is needed so that the measurement is more accurately. The magnification also decreases the sensitivity of the alignment method for artifacts such as PICO, RICO and WICO. Due to the magnification the measurement of the position of the beat pattern is not

very critical. If an error Δ is made in the determination of the beat pattern position this will result in a much smaller error of $(1/M_f)$. Δ in the determination of the fine mark. The magnification factor may be in the order of 10 or 20.

Because the measuring signal is an averaged signal taken from a relatively 5 large substrate surface area, this signal is less sensitive to local surface deformations.

The beat period PE_b can be chosen such that it fits to that of a global mask alignment mark, i.e. an on-axis alignment mark, so that the fine alignment method can be implemented with the on-axis alignment device of Fig.3. After the choice for the beat period has been made, there is still freedom to choose the feature dimensions of the fine alignment 10 marks, i.e. in case of grating marks the periods of these gratings. It is thus possible to optimize the fine substrate mark for minimum sensitivity to process induced deformations. In case of grating marks this means, for example, that the grating period may be of the order of the dimensions of the IC device features, which are to be projected on the substrate by the lithographic apparatus. It is expected that grating marks with such small periods are less 15 vulnerable to said process induced deformations.

The substrate fine alignment mark may be a phase mark and/or an amplitude mark. In case of a phase mark, this mark is etched in a layer of the substrate. The additional, or resist, fine alignment mark is preferably a phase mark. This mark may be constituted by a mark in a developed resist layer. The phase depth of such a mark is determined by the 20 difference in refractive index of the resist and that of the surrounding medium, usually air, and the thickness of the resist. Since this difference in refractive index is fairly large, there is a strong relationship between the resist thickness and the signal strength of the alignment signal. The resist fine alignment mark may also be a so-called latent mark, i.e. an image of a fine alignment mark in a resist that has not been developed. Such image comprises first areas 25 upon which projection beam radiation has been incident and second areas for which this is not the case. These first and second areas provide different optical path length for the alignment-determining beam passing through them. This difference is due to either chemical change in the first areas, which changes cause a change in the refractive index in these areas or to material shrinkage in these areas resulting in a height difference between the first and 30 second areas. These effects are modest and for usual resist thickness no oscillatory change of the alignment signal with resist thickness will occur. Using a latent fine alignment mark provides the advantage that the substrate with the resist layer needs not to be removed from the lithographic apparatus for development of the resist.

If use is made of a latent additional alignment mark a novel alignment strategy can be implemented. This strategy comprises the following steps:

Step 1: a substrate provided with a substrate fine alignment mark and a substrate reference mark and covered with a resist layer is arranged under the projection lens system;

5 Step 2: the substrate is aligned relative to the mask by imaging of the substrate reference alignment mark on a non-substrate reference mark;

Step 3: an additional fine alignment mark is imaged in the resist layer on the area above the substrate fine alignment mark;

10 Step 4: the mutual shift of the substrate fine alignment mark and the additional alignment mark is measured by means of the method described above, whereby the result of this measurement is an indication of an inaccuracy of the alignment device, and

Step 5: use this information, i.e. a correcting factor CF, to correct the alignment.

The substrate reference alignment mark may be a global alignment mark or an alignment mark that belongs to an IC area of the substrate and the non-substrate reference 15 mark may be a mask global alignment mark or a mark outside the mask.

Fig.6 shows a flow diagram of this alignment strategy wherein the steps S₁- S₅ correspond to the above mentioned steps. After this alignment procedure has been carried out the wafer is exposed in the conventional way, i.e. one IC area after the other, which is step 6 in Fig.6. The novel alignment strategy has to be carried out for only one or two wafers per 20 batch.

The new method can be improved by using a spatial, or diffraction order, filter, or diaphragm, which transmits, for example, only the first orders sub-beams from the beat pattern. This filter may be similar to the filter 25 of Fig.3. By such a filter the sensitivity of the alignment measuring method to noise and other disturbances, which may occur in the 25 alignment-measuring device, can be reduced considerably. The advantage of using only the first order sub-beams for imaging the beat pattern on a mask grating is, that the period of the pattern image is half that of the pattern itself, irrespective of the magnification of the projection lens system. As a result, the alignment accuracy is twice as high as in the case that the zero order sub-beam was also used for imaging.

Fig. 7 illustrates diagrammatically the method wherein an order filter 25' is used. In this Figure b is the alignment measuring beam and 75 is a reflector which couples the beam b in the projection column comprising the projection lens system, not shown, of the lithographic apparatus. The optical axis of the projection system coincides with the vertical part of the path of the beam b. The substrate fine alignment mark and the additional mark and

the beat pattern generated by them are schematically represented by the grating structure P_{c_1} which is a composed structure. The sub-beams $b_{Pb}(+1)$ and $b_{Pb}(-1)$ are the alignment beam portions which are diffracted by the grating structure in the plus first diffraction order and the minus first diffraction order, respectively. These sub-beams pass through the openings in the 5 spatial, or order, filter to a mask alignment mark and a detector. The sub-beams of other diffraction orders are blocked by the filter and thus can not reach the detector.

Fig.7 shows also, for illustrative purposes, the sub-beams $b_{P10}(+1)$ and $b_{P10}(-1)$, which, in the embodiment of Fig.5, would be diffracted in the first plus and minus orders by the fine substrate grating P_{10} alone, as well as the sub-beams $b_{P11}(+1)$ and $b_{P10}(-1)$ which would be 10 diffracted in the plus and minus first orders by the additional fine grating P_{11} alone. Due to the small periods of these fine gratings the diffraction angles are so large that these sub-beams even do not enter the projection lens system. This means that the alignment device images only the beat pattern and not an individual fine alignment mark.

The new method can also be used for two-dimensional alignment, i.e. 15 alignment in both the X direction and the Y direction. The substrate fine alignment mark and the additional alignment mark should comprise then both grating strips extending in the Y direction and grating strips extending in the X direction, in a similar way as shown in Fig.2 for the global alignment mark.

Instead of with the alignment device shown in Figures 1 and 3, the novel 20 method can also be performed with other on-axis alignment devices.

The projection system, which is a/o used for imaging the beat pattern on the mask alignment mark may, instead of a lens projection system, also be a mirror system or a system comprising lenses and mirrors. A mirror projection system will be used in an apparatus, such as an EUV apparatus, wherein the projection beam has such a small 25 wavelength that no suitable lens material is available.

The new method may also be implemented with an off-axis alignment measuring device, for example a device by means of which the alignment of a substrate mark relative to a reference is determined and wherein higher-order sub-beams, i.e. sub-beams having a diffraction order which is higher than 1, are used. Since the substrate mark 30 alignment measuring no longer takes place through the projection system, there will be a greater freedom to use more sub-beams, particularly higher-order sub-beams. Since, in general, the resolving power of the alignment- measuring device increases with an increasing order number of the sub-beams, the accuracy of the alignment measuring can be enhanced considerably. Moreover, it is also possible to use alignment-measuring radiation with more

than one wavelength so the requirements imposed on the depth of the grating grooves can be alleviated considerably.

Fig.8 shows the circuit diagram of an off-axis alignment-measuring device. In this Figure the composed substrate grating structure, including the beat pattern, is denoted by 5 P_c . A parallel alignment-measuring beam b having a wavelength λ incident on this structure is split up into a number of sub-beams extending at different angles α_n (not shown) to the normal on the grating, which angles are defined by the known grating formula:

$$\sin \alpha_n = N \cdot \lambda / P$$

10

wherein N is the diffraction order number and P the grating period.. In the path of the sub-beams reflected by the composed grating structure a lens system L_1 is arranged, which converts the different directions of the sub-beams into different positions u_n of these sub-beams in a plane 78:

15

$$u_n = f_1 \cdot \alpha_n$$

In the plane 78 means may be provided for further separating the different sub-beams. To this end, a plate may be arranged in this plane, which is provided with deflection elements in the 20 form of, for example wedges. In Fig.4 the wedge plate is denoted by WEP . The wedges are provided on, for example the rear side of the plate. A prism 77 can then be provided on the front side of the plate, with which the alignment measuring beam coming from the radiation source 76, for example a He-Ne laser can be coupled into the alignment-measuring device. This prism can also prevent the 0-order sub-beam from reaching the detectors. The number of 25 wedges corresponds to the number of sub-beams to be used. In the embodiment shown there are six wedges per measuring direction for the plus orders so that the sub-beams up to and including the 7-order can be used for the alignment measuring. All wedges have a different wedge angle so that an optimal separation of the sub-beams is obtained.

A second lens system L_2 is arranged behind the wedge plate. This lens system 30 images the grating structure P_c in a plane reference plate RGP . In the absence of the wedge plate, all sub-beams would be superimposed on the reference plate. Since the different sub-beams are deflected at different angles by the wedge plate, the images formed by the sub-beams are situated at different positions on the reference plate. These positions x_n are given by:

$$x_n = f_2 \cdot \gamma_n$$

wherein γ is the angle at which a sub-beam is deflected by the wedge plate and f_2 is the focal length of the lens system L_2 . At these positions reference gratings $G_{90} - G_{96}$ (not shown) can be provided, behind each of which a separate detector 90-96 is arranged. The output signal of each detector is dependent on the extent to which the image of the grating structure P_c coincides with the relevant reference grating. Hence the extent of alignment of the substrate grating structure, and thus of the substrate, can be measured with each detector 90-96.

10 However, the accuracy with which the measurement takes place is dependent on the order number of the sub-beam used; as this order number is larger, the accuracy is greater. The grating period of each reference grating is adapted to the order number of the associated sub-beam. As the order number is larger, the grating period is smaller and a smaller alignment error can be detected.

15 Hitherto only one set of diffraction orders has been considered. However, the diffraction structure P_c forms, in addition to +1, +2, +3 etc order sub-beams, also sub-beams of diffraction orders -1, -2, -3 etc. Both the plus orders and minus orders sub-beams can be used to form the grating image, i.e. a first image of the grating structure is formed by the +1 and -1 order jointly, a second image is formed by the +2 and -2 order sub-beams jointly, and

20 so forth. For the +1 order and the -1 order sub-beams no wedges need to be used, but plane-parallel plates which compensate for path-length differences can be provided at the positions of these sub-beams in the plane of the wedge plate. Thus six wedges, both for the plus orders and for the minus orders, are required for the orders 2-7. Also for the alignment measuring in the Y direction seven sub-beams may be used together with seven further reference gratings.

25 A second series of twelve wedges is then arranged on the wedge plate in the Y direction in the embodiment of Fig.8.

For further details and embodiments of the off-axis alignment device wherein different diffraction orders may be used, reference is made to WO 98/ 39689. This patent application describes also under which circumstances the different diffraction orders are used and that alignment radiation having two wavelengths may be used in the off-axis alignment device. The latter provides the advantage that no stringent requirements have to be set on the groove depth of the substrate alignment marks.

With an off-axis alignment-measuring device, for example that of Fig.8, not only the position of a substrate, but also the position of the substrate holder or -table can be

measured. To that end this holder or table is also provided with an alignment mark similar to the global substrate alignment mark. If the position of the substrate holder with respect to the reference in the alignment-measuring device has been determined, the position of the substrate mark with respect to the substrate holder mark will be known. To be able to 5 determine the mutual position of the mask pattern and the substrate, a further measurement is necessary, namely that of the position of the mask pattern with respect to the substrate holder or -table. For this measurement, the on-axis alignment device described with reference to Figures 1 and 3 may be used with which then the position of a mask mark with respect to substrate holder mark is determined. Not only the double alignment-measuring device of 10 Fig.3, but also a single alignment-measuring device as described in US Patent 4,252,160 may be used.

Another possibility of measuring the alignment of the mask pattern with respect to the substrate holder or -table is the use of an image sensor device described in, for example US Patent 4,540,277. In such a device a mask alignment mark is imaged by means 15 of the projection radiation on a corresponding and transmissive reference mark in the substrate table. In this table, a detector may be arranged behind the reference mark for converting radiation passed by the reference mark into an electrical signal. In first instance, this image sensor device was intended for the calibration of an on-axis alignment device which operates with alignment radiation having a wavelength which is considerably different 20 from that of the projection radiation, or for checking the image quality of the image formed by the projection system and for measuring distortions and aberrations which may occur. However, the image sensor is also eminently suitable for measuring the alignment of the mask pattern with respect to the substrate table. Instead of the transmission image sensor device described in US Patent 4,540,277, an image sensor device operating in reflection may 25 be alternatively used for determining the alignment of a mask mark with respect to a substrate table mark. Such a device, which is described in US Patent 5,144,363, operates with a reflective mark on the table and comprises a relatively large numbers of detectors which observe the mark at different angles and which, together with the associated optical systems, are provided in a sensor plate which is arranged between the projection lens system and the 30 substrate table.

The off-axis alignment-measuring device may be arranged in the projection column, comprising the mask holder, the projection system and the substrate holder. With the increasing demands for larger IC's having smaller device features, and thus comprising more electronic components, the alignment procedure becomes more and more time-consuming.

Without further measures, the throughput of lithographic projection apparatus for manufacturing these IC's therefor tends to increase. It has already been proposed to add to such apparatus a separate measuring station. In this station the position in, for example the X-, Y- and Z-direction, of a substrate is measured before this wafer is brought in the projection 5 column, or projection station. In the measuring station substrate marks can be aligned with respect to alignment marks on the substrate holder or table. After the holder with the substrate has been placed in the projection column, only a mask alignment mark needs to be aligned with respect to the substrate holder mark, which takes only a short time. As in the apparatus, comprising a separate measuring station and a projection station, during exposure 10 of a first substrate in the projection station a second substrate is being measured in the measuring station, the throughput of this apparatus is considerably larger than in an apparatus without a separate measuring station. The alignment measuring method of the present invention can be used with advantage in the measuring station.

In practice, the method of the present invention will be applied as one step in a 15 process for manufacturing a device in at least one layer on a substrate, namely for aligning a mask pattern with respect to the substrate before imaging the mask pattern in a resist layer on said layer. After the image has been developed, material is removed from, or added to areas of said layer, which areas are delineated by the printed image. These process steps of imaging and material removing or -adding are repeated for all layers until the whole device is 20 finished.

The invention has been described with reference to its use in an apparatus for imaging a mask pattern on a substrate for manufacturing IC's, but this does not mean that it is limited thereto. The invention may also be used in an apparatus for manufacturing integrated, or planar, optical systems, magnetic heads or liquid crystal panels. The projection apparatus 25 may not only be an optical apparatus, in which the projection beam is a beam of electromagnetic radiation and the projection system is an optical projection lens, or mirror, system, but also in an apparatus wherein the projection beam is a charged-particle beam, such as an electron beam or a ion beam, or an X-ray beam, in which the associated projection system, for example an electron lens system, is used. Generally, the invention may be used in 30 imaging systems with which images having very small details must be formed.

CLAIMS:

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1. A method of measuring alignment of a substrate, provided with at least one substrate alignment mark having a periodic structure, with respect to a reference alignment mark, having a periodic structure, prior to imaging a mask pattern in a resist layer on the substrate, which method comprises the steps of:

5 - illuminating a substrate alignment mark with an alignment beam and imaging this mark on a reference alignment mark, and
- determining the intensity of alignment radiation from the reference alignment mark.

characterized by the steps of:

10 - using a substrate alignment mark having a periodic structure with a period p_1 substantially smaller than the period of the reference alignment mark;
- providing the resist layer with an additional alignment mark having a periodic structure with a period p_2 such that, upon illumination by the alignment beam of the substrate alignment mark and the additional alignment mark, an interference pattern is generated
15 having a period substantially equal to the period of the reference alignment mark, and
- imaging the interference pattern on the reference alignment mark

2. A method as claimed in claim 1 characterized in that, use is made of a substrate reference alignment mark having substantially the same period as the interference pattern, that the substrate reference alignment mark is imaged on the reference alignment mark and in that the difference between the positions of the image of the interference pattern and that of the substrate reference alignment mark with respect to the reference alignment mark are determined.

25 3. A method as claimed in claim 1 or 2, characterized in that use is made of gratings for the substrate-, the additional- and the reference alignment marks.

4. A method as claimed in claim 1, 2 or 3, characterized in that the additional alignment mark is a latent mark.

5. A method of aligning a substrate with respect to a mask using a global alignment measuring method to measure the position of a global substrate alignment mark with respect to a global reference alignment mark, which method is characterized by the steps 5 of:

- providing a substrate with a substrate reference alignment mark and a substrate fine alignment mark having a period substantially smaller than that of the substrate global alignment mark, which substrate is covered with a resist layer;
- aligning the substrate reference alignment mark with respect to a non-substrate 10 reference alignment mark using a coarse alignment measuring method;
- providing the resist layer with an additional alignment mark having a period of the same order as that of the substrate fine alignment mark;
- measuring the alignment of the substrate fine alignment mark with respect to the additional alignment mark by illuminating these two marks and imaging the resulting 15 interference pattern on the non-substrate reference alignment mark, and
- using the measuring signal of this measurement to correct the signal obtained with the coarse alignment method.

6. A method as claimed in any of claims 1-5, characterized in that it is based on 20 the on-axis alignment principle.

7. A method as claimed in claim 6, characterized in that the interference pattern is imaged on a mask alignment mark via an optical filter, which selects diffraction orders of the radiation from the substrate alignment marks to proceed to the said mask alignment mark. 25

8. A method as claimed in any of claims 1-5, characterized in that it is based on the off-axis alignment principle.

9. A method for manufacturing devices in at least one layer of a substrate, which 30 method comprises at least one set of the following steps:

- aligning a mask provided with a mask pattern comprising pattern features corresponding to device feature to be configured in said layer;
- imaging, by means of projection radiation, the mask pattern in a radiation sensitive layer on the substrate, and

removing material from, or adding material to, areas of said layer and substrate, which areas are delineated by the mask pattern image, characterized in that. that the alignment is carried out by means of the alignment measuring method as claimed in any of claims 1-8.

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ABSTRACT:

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For determining the alignment of a substrate (W) with respect to a mask (MA), a substrate alignment mark (P_{10}), having a periodic structure, and an additional alignment mark (P_{11}), having a period structure and provided in a resist layer (RL) on top of the substrate, are used. Upon illumination of these two marks, having a period (PE_{10} ; PE_{11}) 5 considerably smaller than that of a reference mark (M_1 ; M_2) an interference pattern (P_b) is generated, which has a period (PE_b) corresponding to that of the reference mark. By measuring the movement of the interference pattern with respect to the reference mark, the much smaller mutual movement of the fine alignment marks can be measured. In this way, the resolution and accuracy of a conventional alignment device can be increased 10 considerably.

Fig.5

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EPO - DG 1

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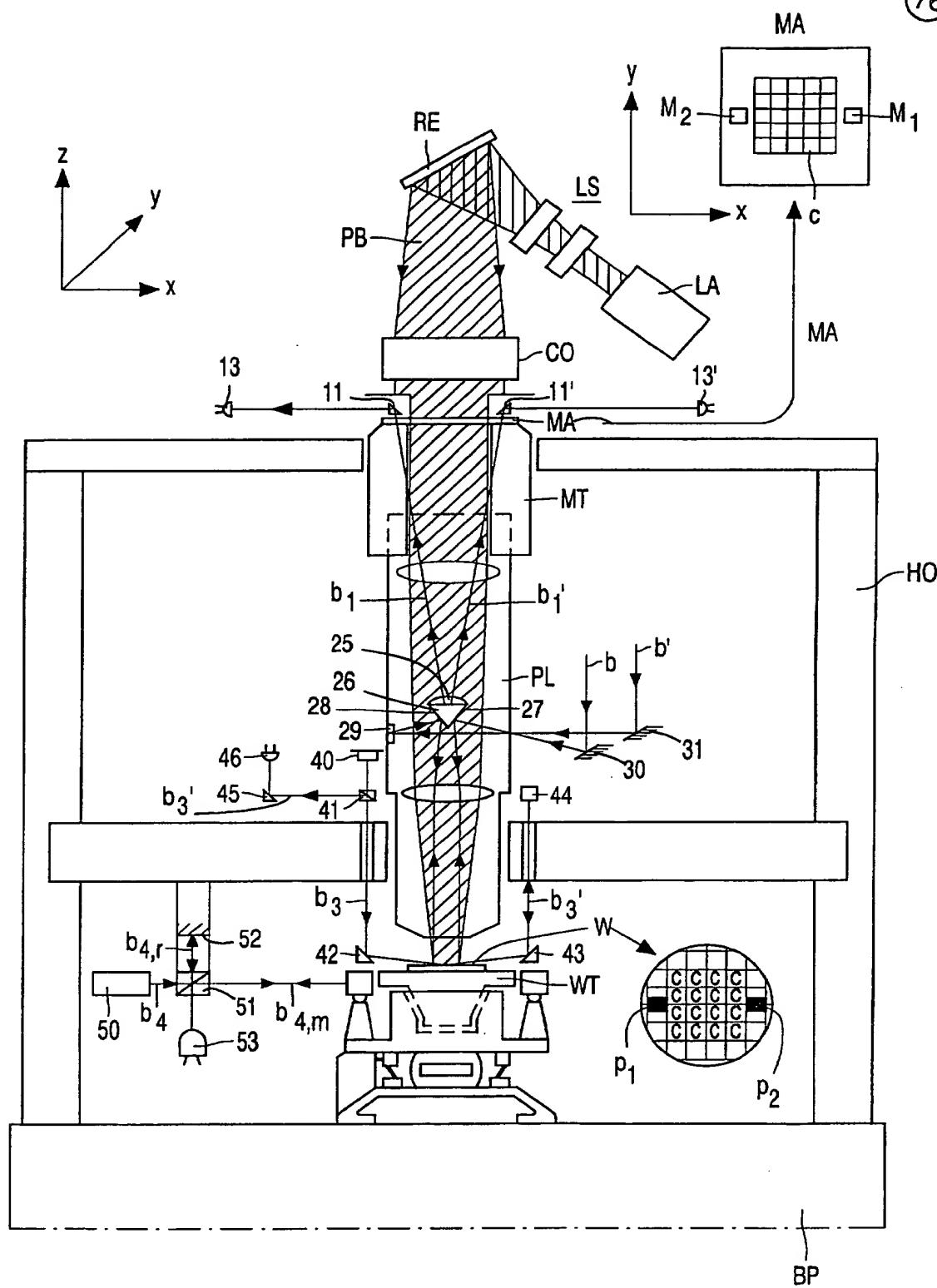


FIG. 1

2/5

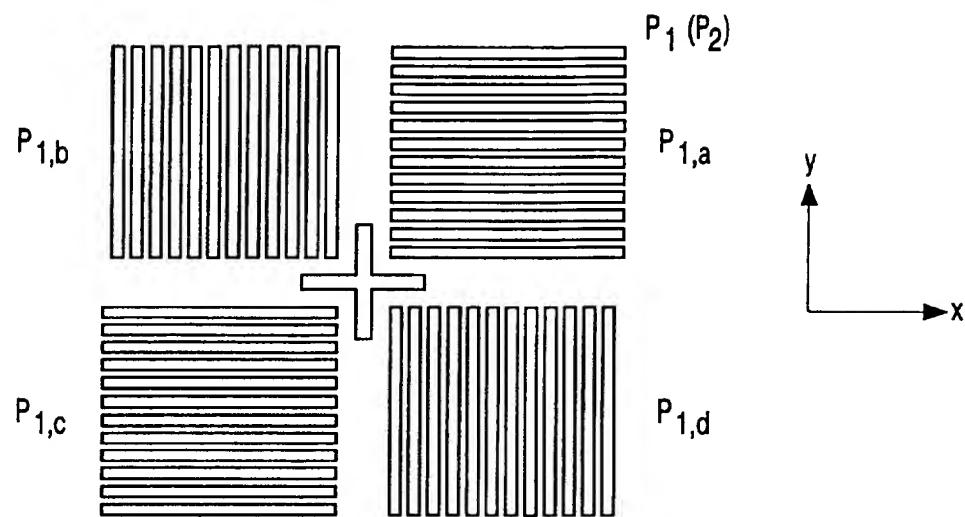


FIG. 2

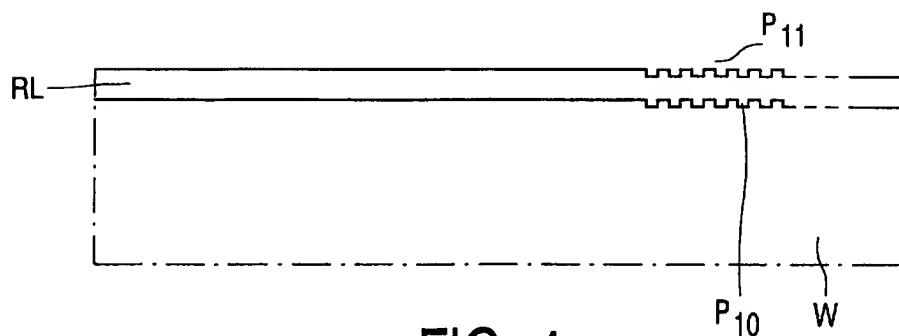


FIG. 4

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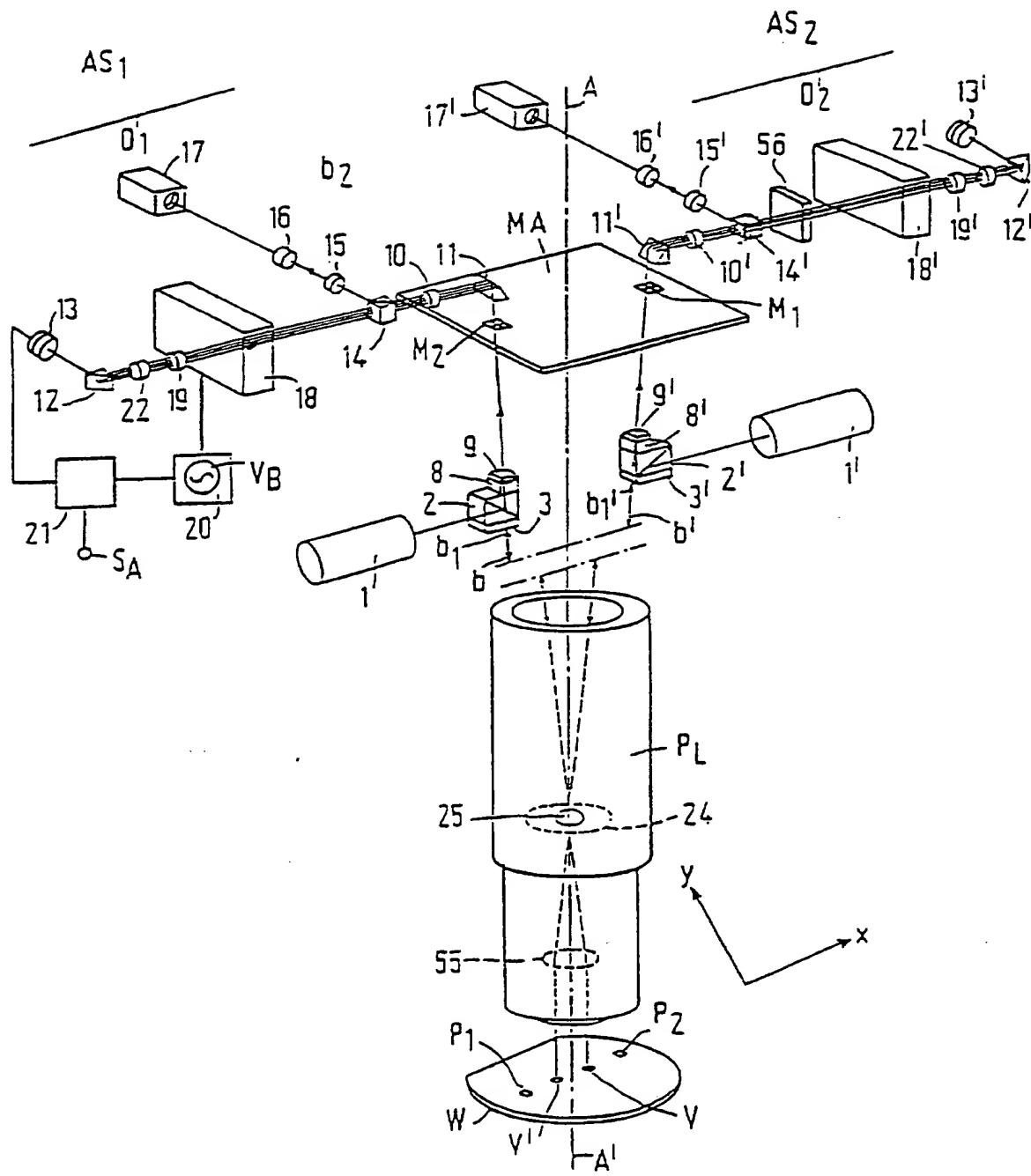


FIG. 3

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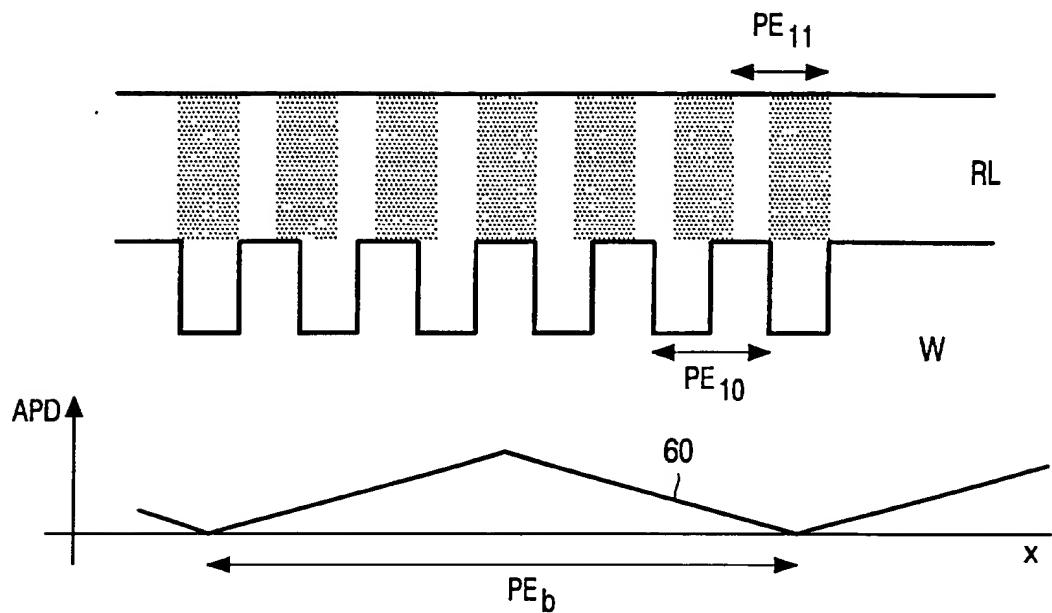


FIG. 5

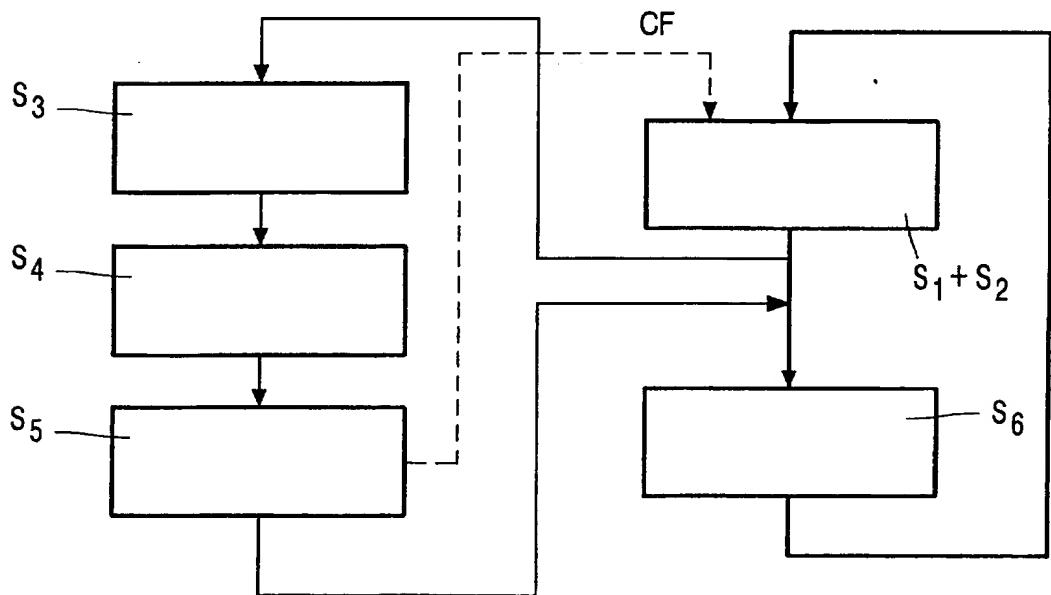


FIG. 6

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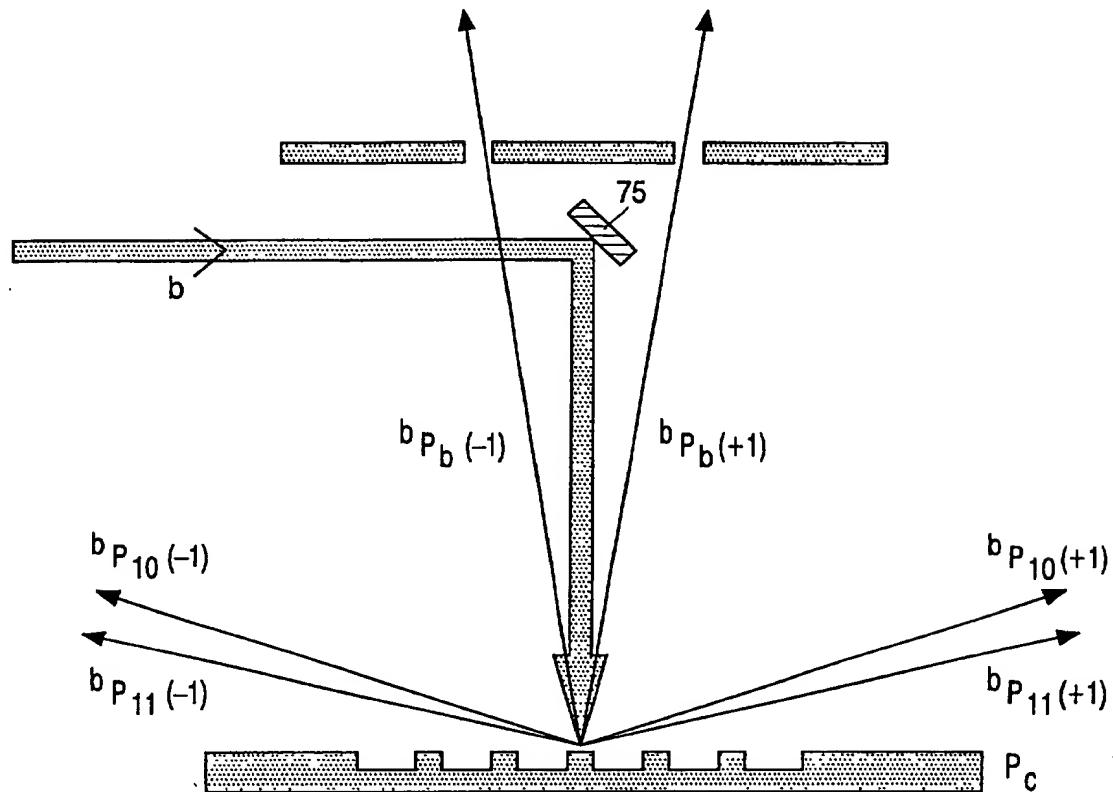


FIG. 7

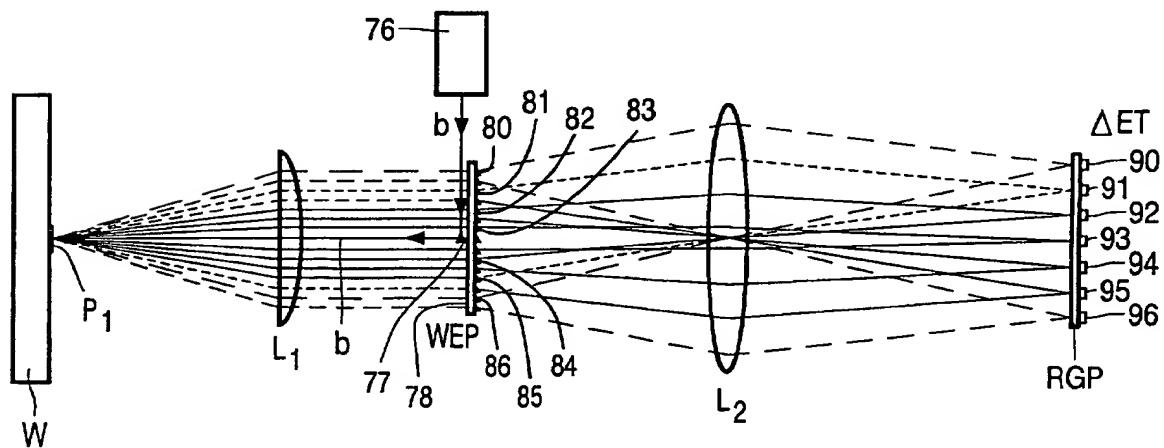


FIG. 8

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